

# EML 3005: GEAR DESIGN EXAMPLE

## SPUR GEAR DESIGN FOR AN AIRCRAFT ENGINE SPEED REDUCER

### Input Design Variables for Gear Mesh # 1

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Gratio1 := 1.285      Gear Ratio      Dpitch1 := 3.5    (pitch dia, in)

$\phi := 20 \cdot \frac{\pi}{180}$       Pressure Angle, 20 deg

Fwidth1 := 1.5      Facewidth, Inch

### Input Duty Cycle for gear mesh (rpm, hp, torque, hours, etc)

N := 9      Number of data points in duty cycle

i := 1..N

HP<sub>i</sub> :=

20
250
278
265
195
200
100
30
20

**Base**

RPM<sub>i</sub> :=

1000
4000
4500
4200
3300
3600
2000
1000
1000

Hours<sub>i</sub> :=

250
25
9
250
1447
510
250
9
250

$$\sum_i \text{Hours}_i = 3000$$

$$\text{Torque}_i := \frac{\text{HP}_i \cdot 33000}{2 \cdot \pi \cdot \text{RPM}_i} \cdot 12 \text{ Inch-lbf}$$

$$\frac{\text{Torque}_i}{12} = \text{ (lb-ft)}$$

105.042
328.257
324.464
331.383
310.352
291.784
262.606
157.563
105.042

$$\text{Torque}_i = \text{ (lbf)}$$

1260.507
3939.085
3893.567
3976.6
3724.226
3501.409
3151.268
1890.761
1260.507

Calculate Tangential Tooth Load

$$\text{Wt1}_i := \frac{\text{Torque}_i \cdot 2}{\text{Dpitch1}} \text{ Lbf}$$

**Print HP, rpm, hours, torque and Wt**

HP <sub>i</sub> =	RPM <sub>i</sub> =	Hours <sub>i</sub> =	in-lbf Torque <sub>i</sub> =	Lbf Wt1 <sub>i</sub> =
20	1000	250	1260.507	720.29
250	4000	25	3939.085	2250.906
278	4500	9	3893.567	2224.895
265	4200	250	3976.6	2272.343
195	3300	1447	3724.226	2128.129
200	3600	510	3501.409	2000.805
100	2000	250	3151.268	1800.724
30	1000	9	1890.761	1080.435
20	1000	250	1260.507	720.29

$$\sum_i \text{Hours}_i = 3000 \quad (\text{Total life required in hours, for gear train})$$

**Calculate equivalent torque and horsepower, for bending and contact loads, for input pinion**

j := 5 (Baseline is for cruise condition)

a1 := 9 (Log S-N curve exponent for contact loads is 9)

a2 := 29 (Log S-N curve exponent for bending loads is 29)

$$\text{Teq}_1 := \left[ \frac{\sum_i \left[ \text{Hours}_i \cdot \text{RPM}_i \cdot (\text{Torque}_i)^{a1} \right]}{\text{RPM}_j \cdot \left( \sum_i \text{Hours}_i - \text{Hours}_j \right)} \right]^{\frac{1}{a1}} \quad \text{Teq}_1 = 3916.421 \quad \text{in-lbf}$$

$$\text{HPeq}_1 := \frac{2 \cdot \pi \cdot \text{RPM}_j \cdot \frac{\text{Teq}_1}{12}}{33000} \quad \text{HPeq}_1 = 205.063$$

### Equivalent torque for CONTACT load

$$T_{eq_1} = 3916.421 \quad \text{in-lbf at} \quad \text{RPM}_j = 3300$$

$$HP_{eq_1} = 205.063 \quad \text{Total number of hours} = \sum_i \text{Hours}_i = 3000$$

### Equivalent loads for bending stress

$$T_{eq_2} := \left[ \frac{\sum_i \left[ \text{Hours}_i \cdot \text{RPM}_i \cdot (\text{Torque}_i)^{a_2} \right]}{\text{RPM}_j \cdot \left( \sum_i \text{Hours}_i - \text{Hours}_j \right)} \right]^{\frac{1}{a_2}} \quad T_{eq_2} = 3843.36 \quad \text{in-lbf}$$

$$HP_{eq_2} := \frac{2 \cdot \pi \cdot \text{RPM}_j \cdot \frac{T_{eq_2}}{12}}{33000} \quad HP_{eq_2} = 201.238$$

### Equivalent torque for BENDING load

$$T_{eq_2} = 3843.36 \quad \text{in-lbf at} \quad \text{RPM}_j = 3300$$

$$HP_{eq_2} = 201.238 \quad \text{Total number of hours} = \sum_i \text{Hours}_i = 3000$$

Calculate bending and contact tangential tooth loads for input pinion 1

$$W_{tbend1} := \frac{T_{eq_2} \cdot 2}{D_{pitch1}} \quad W_{tbend1} = 2196.206 \quad \text{Lbf}$$

$$W_{tcomp1} := \frac{T_{eq_1} \cdot 2}{D_{pitch1}} \quad W_{tcomp1} = 2237.955 \quad \text{Lbf}$$

Equivalent number of stress cycles for Input pinion 1

$$N_{eq} := \left( \sum_i \text{Hours}_i \right) \cdot \text{RPM}_j \cdot 60 \quad N_{eq} = 5.94 \times 10^8$$

## Compute ALLOWABLE bending and contact fatigue stresses in gear teeth

Bending fatigue strength (psi):  
for 9310 gear material  $St := 70000$

Contact fatigue strength (psi):  
for 9310 gear material  $Sc := 225000$

Life factors  $KL := 1.6831 \cdot Neq^{-0.0323}$   $KL = 0.876$

$CL := 2.466 \cdot Neq^{-0.056}$   $CL = 0.796$

### Allowable Bending and Contact Stresses

$\sigma_{all} := St \cdot KL$   $\sigma_{all} = 61350.013 \text{ psi}$

$\sigma_{call} := Sc \cdot CL$   $\sigma_{call} = 178996.092 \text{ psi}$

## Calculate ACTUAL bending and contact stresses in pinion teeth

Elastic constant (psi):  $Cp := 2300$

Mounting factors:  
Precise mounting  $Cm := 1.3$

$Km := 1.3$

Quality factor, around 10 for heat treated  
and ground gears  $Qv := 10$

Hardness factors  $CR := 1$

$KR := 1$

### Calculate velocity factor

Pitch line velocity in Ft/min:  $V := \frac{\pi \cdot D_{pitch1} \cdot RPM_j}{12}$   $V = 3023.783$

Compute constants A & B  $B := \frac{(12 - Qv)^{\frac{2}{3}}}{4}$   $A := 50 + 56 \cdot (1 - B)$

Velocity Factor  $Kv := \left( \frac{A}{A + \sqrt{V}} \right)^B$   $Kv = 0.819$

## CALCULATE OPTIMUM NUMBER OF TEETH, Np

### Geometric Factors

$$I_1 := \frac{\cos(\phi) \cdot \sin(\phi)}{2} \cdot \frac{\text{Gratio1}}{\text{Gratio1} + 1} \quad I_1 = 0.09$$

$$J_1 := 0.43(\text{Guess})$$

$$N_p := \frac{\sigma_{\text{all}} \cdot J_1 \cdot C_p^2}{\sigma_{\text{call}}^2 \cdot I_1} \quad N_p = 48.198$$

Choose Np at 48 teeth:  $N_p := 48$

$$P_d1 := \frac{N_p}{D_{\text{pitch1}}} \quad P_d1 = 13.714$$

Note: The nearest standard Pd is 12, which will give 42 teeth. Lets stay with 48 teeth.

### Calculate Pinion Facewidth

$$\sigma_{\text{all}} = 61350.013$$

$$F_{\text{bend}} := \frac{W_{\text{tbend1}} \cdot P_d1 \cdot K_m}{\sigma_{\text{all}} \cdot K_v \cdot J_1} \quad F_{\text{bend}} = 1.813$$

$$F_{\text{cont}} := \frac{W_{\text{tcomp1}} \cdot C_m \cdot C_p^2}{K_v \cdot I_1 \cdot D_{\text{pitch1}} \cdot \sigma_{\text{all}}^2} \quad F_{\text{cont}} = 1.855$$

Choose facewidth as 1.9 inches:  $F_{\text{width}} := 1.9$

### Tooth bending and contact stresses are (check):

$$\sigma_{\text{bend}} := \frac{W_{\text{tbend1}} \cdot P_d1 \cdot K_m}{F_{\text{width}} \cdot K_v \cdot J_1} \quad \sigma_{\text{bend}} = 58551.897 \quad \text{psi}$$

$$\sigma_{\text{cont}} := C_p \cdot \sqrt{\frac{W_{\text{tcomp1}} \cdot C_m}{K_v \cdot I_1 \cdot D_{\text{pitch1}} \cdot F_{\text{width}}}} \quad \sigma_{\text{cont}} = 176884.12 \quad \text{psi}$$

Allowable stresses are:  $\sigma_{\text{all}} = 61350.013$   $\sigma_{\text{call}} = 178996.092$

Numbers look O.K

$$\# \text{ gear teeth} \quad N_g := N_p \cdot \text{Gratio1} \quad N_g = 61.68$$

Choose Ng, the number of teeth on gear 2, as 62

$$N_g := 62$$

$$\text{Actual gear ratio is:} \quad M_g := \frac{N_g}{N_p} \quad M_g = 1.292$$

## GEAR DESIGN SUMMARY FOR MESH 1

$$Pd1 = 13.714 \text{ teeth/in}$$

$$Np = 48$$

$$St = 70000$$

$$Ng = 62$$

$$Sc = 225000$$

$$Mg = 1.292$$

$$Fwidth = 1.9$$

$$\sigma_{bend} = 58551.897$$

$$\sigma_{all} = 61350.013$$

$$\sigma_{cont} = 176884.12$$

$$\sigma_{call} = 178996.092$$

Factor of safety:

$$FOS_{bend} := \frac{\sigma_{all}}{\sigma_{bend}} \quad FOS_{bend} = 1.048$$

$$FOS_{cont} := \frac{\sigma_{call}}{\sigma_{cont}} \quad FOS_{cont} = 1.012$$

### Pinion life with 1.9 inch facewidth

$$KL_{new} := \frac{\sigma_{bend}}{St} \quad KL_{new} = 0.836$$

$$CL_{new} := \frac{\sigma_{cont}}{Sc} \quad CL_{new} = 0.786$$

$$exp1 := \frac{\log(1.6831) - \log(KL_{new})}{0.0323} \quad exp2 := \frac{\log(2.466) - \log(CL_{new})}{0.056}$$

### BENDING LIFE

$$N_{bend} := 10^{exp1} \quad N_{bend} = 2.52 \times 10^9 \quad (\text{bending life, cycles})$$

$$Bendlife := \frac{N_{bend}}{60 \cdot RPM_j} \quad Bendlife = 12728.866 \quad (\text{bending life, hours})$$

### CONTACT LIFE

$$N_{cont} := 10^{exp2} \quad N_{cont} = 7.342 \times 10^8 \quad (\text{contact life, cycles})$$

$$Contlife := \frac{N_{cont}}{60 \cdot RPM_j} \quad Conlife = 3708.255 \quad (\text{contact life, hours})$$

**LIFE OF GEARMESH #1 = 3708 HOURS**